Effect of I/E ratio on mean alveolar pressure during high-frequency oscillatory ventilation

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Pillow, J. J., H. Neil, M. H. Wilkinson, and C. A. Ramsden. Effect of I/E ratio on mean alveolar pressure during high-frequency oscillatory ventilation. J. Appl. Physiol. 87(1): 407–414, 1999.—This study investigated factors contributing to differences between mean alveolar pressure (PA) and mean pressure at the airway opening (Pao) during high-frequency oscillatory ventilation (HFOV). The effect of the inspiratory-to-expiratory time (I/E) ratio and amplitude of oscillation on the magnitude of PA – Pao (Pdiff) was examined by using the alveolar capsule technique in normal rabbit lungs (n = 4) and an in vitro lung model. The effect of ventilator frequency and endotracheal tube (ETT) diameter on Pdiff was further examined in the in vitro lung model at an I/E ratio of 1:2. In both lung models, PA fell below Pao during HFOV when inspiratory time was shorter than expiratory time. Under these conditions, differences between inspiratory and expiratory flows, combined with the nonlinear relationship between resistive pressure drop and flow in the ETT, are the principal determinants of Pdiff. In our experiments, the magnitude of Pdiff at each combination of I/E, frequency, lung compliance, and ETT resistance could be predicted from the difference between the mean squared inspiratory and expiratory velocities in the ETT. These observations provide an explanation for the measured differences in mean pressure between the airway opening and the alveoli during HFOV and will assist in the development of optimal strategies for the clinical application of this technique.

high-frequency ventilation; gas trapping; lung volume; mean airway pressure

THE POSSIBILITY THAT GAS TRAPPING may occur during high-frequency oscillatory ventilation (HFOV) has been a source of concern for many years. This concern has been heightened by perceived similarities with conventional mechanical ventilation, where it is well recognized that gas trapping can occur at high ventilator rates (17, 18, 20).

During conventional mechanical ventilation (CMV), the time required for pressure to equilibrate between the alveolar space and the patient’s airway, and thus for inspiration or expiration to be complete, is determined by the time constant, which is the product of compliance (C) and resistance (R) of the respiratory system. Because expiratory resistance is commonly up to fourfold greater than inspiratory resistance (17), application of rapid ventilator rates during CMV may easily compromise expiration. Gas trapping results, with elevation of alveolar pressure above airway pressure at end expiration, in a phenomenon commonly referred to as inadvertent positive end-expiratory pressure (3, 17, 20). To minimize the risk of this problem occurring during CMV at rapid rates, inspiratory-to-expiratory time (I/E) ratios of at least 1:2 are commonly employed.

Extrapolation of the principles underlying choice of I/E ratio for CMV has led many authorities to also recommend the use of I/E ratios of at least 1:2 for HFOV, with the same intent of avoiding gas trapping and the associated dangers of hyperinflation, air leak, and cardiovascular compromise. The extent to which gas trapping occurs during HFOV, elevating mean alveolar pressure (PA) above mean airway opening pressure (Pao), remains controversial. Various investigators have reported that global or regional measures of PA may be the same (1, 5), higher (1, 2, 5, 7, 13, 19, 21), or lower (13, 25) than Pao during HFOV. Differences in ventilator settings including I/E ratio (13), Pao (5), ventilator amplitude (I/Pao) (1), and the effects of regional factors (1) and posture (1, 21) appear to account, at least in part, for these disparate observations.

To date, there has been no quantitative description of the effect of oscillatory ventilator settings and mechanical characteristics of the lung on the difference (Pdiff) between PA and Pao. This study was, therefore, undertaken to systematically examine the interaction of key ventilatory parameters on the magnitude of Pdiff in the lungs of young rabbits and in an in vitro lung model.

MATERIALS AND METHODS

Experiments were performed on the lungs of four adult rabbits and an in vitro model of the intubated newborn respiratory system. Animal experiments were performed in accordance with the guidelines of the Australian National Health and Medical Research Council and with the approval of the Animal Ethics Committees of Monash Medical Centre and Monash University (approval no. A9452).

Lung Models

Rabbit lung model. Four adult New Zealand White rabbits (body weight, 4.0 ± 1.8 kg) were administered a lethal dose of pentobarbital sodium (160 mg/kg) and intubated through a tracheostomy with an 11-cm-long, 3.0-mm-ID endotracheal tube (ETT) (Portex, UK). Intermittent positive pressure ventilation of the lungs (peak inspiratory pressure = 15 cmH2O; end-expiratory pressure = 5 cmH2O; rate = 30 breaths/min; inspiratory time = 0.7 s) was initiated with a Humming II ventilator (Senko Medical Instrument Manufacturing, Japan) and maintained until the completion of surgical procedures when HFOV was commenced with a SensorMedics 3100 high-frequency oscillator. To measure alveolar pressure (PA) by the alveolar capsule technique (12, 13), a right thoracotomy was performed and a small plastic capsule glued (Supaglue, Selleys Chemical, Australia) to the exposed anterolateral surface of the right middle (n = 3) or

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right lower (n = 1) lobe of the lung. The pleural surface enclosed within the capsule was punctured in five places with a 23-gauge needle inserted to a uniform depth (2 mm). The capsule opening was then sealed by inserting the tip of a Micron MP15 pressure transducer (Micron Instruments), which was carefully supported to exert minimal pressure on the underlying lung.

The capsule was confirmed to be free of leaks by demonstrating that P_A remained constant after airway occlusion at end inspiration. Immediately before HFOV was commenced, the C and R of the respiratory system were determined by the airway-occlusion technique (16) by using a Hans Rudolph no. 1 pneumotachograph. Mean (± SD) C was 2.67 ± 0.64 ml/cmH_2O, and mean R was 250 ± 0.13 cmH_2O·s·l^{-1}.

In vitro lung model. To simulate the mechanical properties of the respiratory system of the intubated human newborn infant suffering from hyaline membrane disease, we employed a lung model comprising an 11-cm-long, 3.0-mm-ID ETT, sealed into the neck of a 590-ml glass flask (see Fig. 1). The model had an adiabatic compliance C of 0.4 ml/cmH_2O and an R of 75 cmH_2O·s·l^{-1} [measured at a flow (V) = 0.1 l/s].

Measurement of Pressure

P_A and pressure at the airway opening (Pao), Pao was measured with a Micron MP15 pressure transducer (Micron Instruments) via a sideport positioned immediately above the connection to the ETT and perpendicular to the ventilator tubing. Pressure in the interior of the in vitro lung model (P_A) was also measured with an MP15 transducer positioned at the end of an 11-cm-long, 12-gauge needle inserted into the glass flask. Similar measurements of mean pressure were obtained when Pao was measured at other sites close to the airway opening and when P_A was determined at a variety of sites within the glass flask (results not shown).

![Fig. 1. In vitro lung model. Pao, pressure at airway opening; P_A, alveolar pressure; ETT, endotracheal tube.](image)

The time constant of the MP15 transducer response to a sudden change in pressure by balloon-burst testing was 0.7 ms for the MP15 transducer alone and 2.6 ms for the MP15-needle combination, indicating a frequency response that was adequate up to at least 454 and 134 Hz, respectively, for Pao and P_A measurements. The output of the MP15 was linear over the range ~70 to +140 cmH_2O. Transducer signals were amplified and low-pass filtered at 400 Hz (Cyberamp 320, Axon Instruments), digitized at 1 kHz, and stored on a personal computer by using data-acquisition software (Spike 2, Cambridge Electronic Design, UK).

Mean pressures. Measurements of mean pressures were determined from the average of at least 10 complete cycles of oscillation. The potential for errors arising from differences in transducer calibration when determining differences between P_A and Pao was eliminated in the in vitro lung model by measuring P_A and Pao with the same transducer connected either to the airway opening or to the interior of the lung. In the rabbit lung, each transducer was carefully calibrated to the same gain. Potential errors arising from zero drift were minimized by frequently referencing each transducer to the same static pressure, achieved by briefly reducing the amplitude of the pressure oscillation delivered by the high-frequency ventilator to zero.

Amplitude of pressure oscillation at the airway opening ΔPao. Reporting of the amplitude of pressure oscillation produced by the SensorMedics 3100 at the airway opening is confounded by the waveform’s complex shape, which approximates to a square wave, upon which are superimposed large-amplitude, damped oscillations at the onset of both inspiration and expiration. Where observations were made at various amplitudes, we have reported the amplitude displayed by the ventilator. The ventilator internal pressure measurement provides a damped estimate of the amplitude ΔPao, since the pressure transducer is placed at the end of a 75-cm length of 3.5-mm-bore tubing attached to the inspiratory limb of the ventilator circuit, 1 cm before the patient’s airway connection. Consequently, the ΔPao displayed by the ventilator approximates the amplitude of the square-wave component of the pressure waveform.

Calculation of tidal volume (VT) and V’. In the in vitro lung model, VT was calculated by using the equation

\[ VT = \frac{V_L \cdot \Delta P_A}{\gamma \cdot P_0} \]  

(1)

where \( V_L \) is model lung volume, \( \Delta P_A \) is amplitude of oscillatory pressure waveform in the model lung, \( P_0 \) is atmospheric pressure, and \( \gamma \) is adiabatic gas constant (1.4 for air). \( V’ \) was calculated throughout the oscillatory cycle by using numerical differentiation such that

\[ V’ = C \cdot \frac{dP_A}{dt} \]  

(2)

where C is model lung compliance and \( P_A \) is the instantaneous pressure in the model lung.

Experimental Protocols

In all experiments, HFOV was delivered by a SensorMedics 3100 high-frequency oscillator, operated in accordance with the manufacturer’s instructions. All observations were made at a mean airway pressure of 10 cmH_2O.
Pao could be identified in the rabbit lung model during HFOV and to investigate the effect of the I/E ratio on these differences. By using a ventilator frequency of 15 Hz, the magnitude of Pdiff was determined at I/E ratios of 1:1 and 1:2 across a range of Dpao from a minimum of 10 cmH2O to a maximum of 90 cmH2O. Two observations were made at each setting, and average values of Pdiff were determined for individual rabbits at each Dpao and I/E ratio.

Pdiff in the in vitro lung model. Experiments were performed to test whether differences between PA and Pao could be identified in the in vitro lung model and to examine the independent effects of ventilator amplitude, frequency, and I/E ratio as well as the model lung compliance and ETT resistance on those differences. The range of ventilator settings examined and the characteristics of the lung model employed in each protocol are summarized in Table 1. Ventilator settings were changed in random sequence until triplicate observations of PA and Pao had been made under each experimental condition. Differences between PA and Pao were pooled to determine average values for Pdiff.

Statistical Analysis

Results are shown as means ± SE. Statistical analysis of the data derived from the rabbit experiments was complicated by the unequal number of measurements of Pdiff obtained across a range of ventilator amplitudes in each rabbit. A multilevel modeling approach using a nested hierarchical design was employed (statistical software MLn v 1.0a, Institute of Education, London, UK). Constant variance was assumed. Two levels were employed in the analysis to account for differences between the observations of Pdiff made at different amplitudes (level 1) and between rabbits (level 2). Data at each I/E ratio were assessed separately.

RESULTS

Pdiff in the Rabbit Lung

The measurements of Pdiff made during HFOV in each of the rabbit lungs are illustrated in Fig. 2A. In the rabbit lung, Pdiff was not significantly different from zero (maximum −0.8 ± 0.3 cmH2O) at an I/E ratio of 1:1. However, at an I/E ratio of 1:2, PA was substantially less than Pao, and the magnitude of Pdiff increased with the square of the oscillatory pressure amplitude at the patient’s airway to a maximum value of 25.0 ± 0.2 cmH2O.

Pdiff in the In Vitro Lung Model

As in the rabbit lung Pdiff in the in vitro lung was <1 cmH2O at an I/E ratio of 1:1 (Fig. 2B). In contrast to the rabbit lung, however, Pdiff was positive (PA > Pao), and a statistically significant difference in Pdiff was demonstrable between models for amplitudes in excess of 30 cmH2O. At an I/E ratio of 1:2, PA was substantially less than Pao (maximum difference −6.6 ± 0.2 cmH2O), and the difference increased with increasing amplitude in a similar manner to the rabbit lung.

Figure 3 illustrates the effect of changing the amplitude, frequency, and I/E ratio of the ventilator and both

Table 1. Ventilator settings and in vitro lung model characteristics

<table>
<thead>
<tr>
<th>Protocol</th>
<th>Ventilator Settings</th>
<th>Lung Model</th>
</tr>
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<tbody>
<tr>
<td></td>
<td>Amplitude, cmH2O</td>
<td>Frequency, Hz</td>
</tr>
<tr>
<td>Effect of amplitude</td>
<td>10–90*</td>
<td>15</td>
</tr>
<tr>
<td>Effect of frequency</td>
<td>10–90*</td>
<td>7.5, 10, 15</td>
</tr>
<tr>
<td>Effect of I/E ratio</td>
<td>70†</td>
<td>15</td>
</tr>
<tr>
<td>Effect of ETT diameter</td>
<td>10–90*</td>
<td>15</td>
</tr>
<tr>
<td>Effect of compliance</td>
<td>80</td>
<td>15</td>
</tr>
</tbody>
</table>

ETT ID, internal diameter of endotracheal tube. *Amplitude was adjusted in steps of 10–15 cmH2O. †Amplitude was adjusted at each setting of inspiratory-to-expiratory time (I/E) ratio to deliver a calculated tidal volume of 7 ml. ‡Inspiratory time, expressed as a percentage of total cycle time, was adjusted in steps of 2–3% between 30% (I/E = 1:2.3) and 50% (I/E = 1:1). §Compliance was varied by filling a 3.1-liter flask with measured volumes of water.
the ETT diameter and compliance of the lung model, on the magnitude of $P_{\text{diff}}$. An increase in ventilator frequency (Fig. 3A) at an I/E ratio of 1:2 or reduction of the inspiratory time as a fraction of total cycle time (Fig. 3B) caused $P_A$ to fall progressively below $P_{ao}$. Reduction in the resistance of the lung model, by increasing ETT diameter, decreased $P_{\text{diff}}$ at a given VT (Fig. 3C), whereas a change in compliance had negligible effect (Fig. 3D) until very low compliances were reached ($\leq 0.5\, \text{ml/cmH}_2\text{O}$), after which $P_{\text{diff}}$ fell rapidly with decreasing compliance.

**DISCUSSION**

In common with several previous publications (1, 6, 19, 21), we found evidence in this study that $P_A$ may differ significantly from $P_{ao}$ during HFOV and that I/E ratio is a crucial determinant of whether such a difference is present. The novel feature of our study is that it represents the first systematic evaluation of the effects of individual HFOV settings, and the influence of mechanical properties of the lung, on the magnitude of differences between $P_A$ and $P_{ao}$. We found no evidence of significant gas trapping ($P_A > P_{ao}$) at an I/E ratio of 1:1. Rather, differences between $P_A$ and $P_{ao}$ of sufficient magnitude to be of potential clinical significance ($\geq 1\, \text{cmH}_2\text{O}$) were seen only at an I/E ratio of 1:2 and were opposite in sign ($P_A < P_{ao}$). Interestingly, differences between $P_A$ and $P_{ao}$ (i.e., $P_{\text{diff}}$) could be elicited even in a very simple in vitro lung model, where their magnitude was very similar to that seen in whole rabbit lung oscillated at comparable settings, suggesting that the ETT itself is critical to the generation of $P_{\text{diff}}$.

**Critique of Methods**

Our in vitro and animal lung models were chosen because their mechanical properties resemble the human newborn infant's respiratory system. Thus the compliance of the in vitro model (0.4 ml/cmH$_2$O) was comparable to that seen in severe hyaline membrane disease (13), a condition for which HFOV is commonly employed. We also used a range of ETTs (ID 2.5–3.5 mm) that spanned the range of sizes normally used for human newborn infants. However, although the total resistance of the intubated neonatal respiratory system has a significant contribution from the ETT (11), our in vitro model lacked conducting airways beyond the ETT, and its resistance must therefore have been less than that in the human newborn. Again, the rabbit was chosen as our whole lung model for its similarity in size.
and mechanical properties to the human newborn infant.

Measurements of $P_A$ in the rabbit lung were made with the alveolar capsule technique, which has been used previously by several investigators to measure $P_A$ during high-frequency ventilation (1, 11–13). This technique has been demonstrated by Gerstmann and colleagues (13) to potentially overestimate $P_A$ when capsule and transducer are relatively heavy. We attempted to minimize this problem in our experiments by carefully supporting the pressure transducer to achieve a near-weightless condition. Whereas we cannot exclude the presence of some residual effect, we note that by causing overestimation of $P_A$ such an effect would have tended to lessen the $P_{\text{diff}}$ that we observed at an I/E ratio of 1:2. Employing a single alveolar capsule, we were unable to examine whether any regional variation in $P_A$ was present in our experiments. However, when regional variation is present, $P_A$ is usually lowest in the upper lobe of the lung during HFOV (1, 13), and our choice of the middle or lower lobe for alveolar capsule placement would again have tended to give a minimum estimate of the magnitude of the $P_{\text{diff}}$ present at an I/E ratio of 1:2.

Although measurement of static pressure is relatively uncomplicated, several investigators have previously noted that pressure measurements in a moving stream of gas may underestimate the driving pressure because of the Bernoulli effect (4, 8). In our measurement system, the most likely pressure to be affected by a Bernoulli effect was $P_\text{ao}$; however, the worst-case calculated dynamic pressure at that site was $\leq 0.1$ cmH$_2$O.

**Difference Between $P_A$ and $P_\text{ao}$**

In contrast to our finding of no more than small differences ($\leq 1$ cmH$_2$O) between $P_A$ and $P_\text{ao}$ in both the rabbit and in vitro lung models at an I/E ratio of 1:1, several previous studies in dogs (21), rabbits (13), and adult human subjects (19, 23) have each shown a potential for $P_A$ to be significantly elevated above $P_\text{ao}$ when HFOV was employed at an I/E ratio of 1:1. A number of mechanisms have been postulated to account for this effect, and each depends on the presence of asymmetry between inspiratory and expiratory resistance. They include changes in airway caliber between inspiration and expiration (15) that may be particularly evident at low lung volumes (low $P_\text{ao}$) and the effects of flow separation at branch points in the airway (6). Bryan and Slutsky (5) have suggested, however, that the elevation of $P_A$ above $P_\text{ao}$, observed in the study of Saari and colleagues (19) and that of Simon and co-workers (21), might alternatively be explained by the development of "choke points" that cause expiratory flow limitation at low $P_\text{ao}$. In support of their hypothesis, they found the level of $P_\text{ao}$ to be the crucial determinant of whether gas trapping occurred in normal or surfactant-depleted rabbits given HFOV at an I/E ratio of 1:1.

The various potential sources of asymmetry between expiratory and inspiratory resistance ($R_{\text{e}}$ and $R_{\text{i}}$, respectively) outlined above each cause $R_{\text{e}}$ to exceed $R_{\text{i}}$, and, in turn, have the capacity to cause $P_A$ to exceed $P_\text{ao}$. None, however, explains the observations made in our study where we saw minimal elevation of $P_A$ above $P_\text{ao}$ at a 1:1 ratio in the in vitro lung and no elevation at all in the rabbit lung, where such sources of asymmetry would have been most likely to be evident. The lack of evidence of $P_A$ exceeding $P_\text{ao}$ may well be explained by the observation made by Byran and Slutsky (5) that the level of $P_\text{ao}$ is a the crucial determinant of whether gas trapping occurred in normal or surfactant-depleted rabbits given HFOV at an I/E ratio of 1:1. Our studies employed a $P_\text{ao}$ of 10 cmH$_2$O, which is well above that employed in those earlier studies in which gas trapping was seen (1, 6, 17, 25, 28) but is no higher than the minimum $P_\text{ao}$ commonly employed in the clinical setting.

By contrast, the striking finding in our study was that, at an I/E ratio of 1:2, $P_A$ may fall substantially below $P_\text{ao}$. Several years ago, Gerstmann et al. (13) made a similar observation that the average tracheal pressure may be less than $P_\text{ao}$ during HFOV in the rabbit at an I/E ratio of 1:2, and more recently Hatcher et al. (14) have found that $P_A$ determined by airway occlusion may be less than $P_\text{ao}$ at an I/E ratio of 1:2. The lower value of $P_A$ compared with $P_\text{ao}$ may again be accounted for by asymmetry between $R_{\text{e}}$ and $R_{\text{i}}$, but requires the unusual situation to arise, whereby $R_{\text{e}}$ exceeds $R_{\text{i}}$, which is the converse of the relationship when $P_A$ is higher than $P_\text{ao}$. Our data provide evidence that turbulence in the ETT, as first suggested by Gerstmann et al. (13), can account for this phenomenon.

**Turbulence and $P_{\text{diff}}$**

During HFOV, one may predict that the high inspiratory and expiratory flows are likely to be associated with turbulence in the ETT. We may, therefore, expect that both the resistance $R$ and the resistive pressure drop ($P_{\text{res}}$) along the ETT can be predicted from Rohrer’s equation, such that $R = k_1 + k_2V^2$ and $P_{\text{res}} = k_1V + k_2V^2$. If we assume that the values of $k_1$ and $k_2$ are similar in inspiration and expiration, we can then predict the effect of changes in inspiratory or expiratory flow $V’$ on the magnitude of $P_{\text{res}}$ during inspiration and expiration (see APPENDIX A).

In the simple circumstance of an I/E ratio of 1:1, the average inspiratory flow $V_1$ must equal the average expiratory flow $V_2$, and both the resistance and $P_{\text{res}}$ during inspiration and expiration will be equal. In our in vitro lung model at least, with no airways beyond the ETT, we would therefore expect $P_A$ to equal $P_\text{ao}$. In contrast, at an I/E ratio of 1:2, the average inspiratory flow $V_1’$ must be twice the average expiratory flow $V_2’$, since it is sustained for only half the time. As $P_{\text{res}}$ depends on the square of $V’$ under turbulent flow conditions, the average $V_1’^2$ will be four times greater than the average $V_2’^2$. The effect on $P_{\text{res}}$ of doubling inspiratory flow with respect to expiratory flow will therefore exceed the countering effect on $P_{\text{res}}$ of expiratory time doubling, relative to inspiratory time. Thus,
at an I/E ratio of 1:2, the unusual circumstance whereby Ri is greater than Re arises, such that the inspiratory P_{res} must exceed the expiratory P_{res}, with the inevitable consequence that PA must fall below Pao in our in vitro lung model. In more general terms, we can predict that, at any I/E ratio other than 1:1, PA will deviate from Pao, and the magnitude of that deviation will be directly proportional to the difference between the mean squared inspiratory (U_I^2) and expiratory velocities (U_E^2) in the ETT (see Appendix A).

To test the capacity of this model to explain the magnitude of P_{diff} in our in vitro lung model, we have plotted each measurement of P_{diff} in Fig. 3 against the corresponding difference between U_I^2 and U_E^2, which we determined (knowing the in vitro lung compliance) by differentiating the pressure change within the flask (see Fig. 4). The correlation between P_{diff} and (U_I^2 - U_E^2) was very close (r^2 = 0.95), suggesting that the effect of turbulence could largely account for the P_{diff} seen in our in vitro lung model. Furthermore, the close similarity between the results obtained in the in vitro lung model and those obtained in the rabbit strongly suggests that, even in the whole lung, events occurring in the ETT may be the principal determinant of differences between PA and Pao.

In deriving the relationship between P_{diff} and U_I^2 - U_E^2, we have assumed that the values of k_1 and k_2 during inspiration are equal to those during expiration. Sly et al. (22) have published k_1 and k_2 values measured during steady flow for a number of ETT values ranging in size from 2.5 to 5.5 mm ID. Their observations suggest that k_1 and k_2 during expiration are slightly higher than during inspiration, by ~10%, in agreement with differences in the inspiratory and expiratory ETT flow profiles observed by Chang and Mortola (9). Such a small increase of expiratory resistance relative to inspiratory resistance could account for the small elevation of PA above Pao in our in vitro lung model at an I/E ratio of 1:1. A further point of interest is that the calculated slope of the relationship between P_{diff} and U_I^2 - U_E^2 is -0.012, which is in good agreement with the theoretically predicted slope (−0.013) calculated from the experimental data of Sly et al. (22) (see Appendix A).

Clearly, these conclusions are predicated on the assumption that parameters measured from steady-flow experiments are applicable in the high-frequency oscillation setting. Only further experimental work directed at measuring k_1 and k_2 during oscillatory flow can resolve this issue.

Clinical Implications

Although a substantial P_{diff} was only seen at relatively high ventilator pressure amplitudes in these experiments, it should be noted that the resistance of our in vitro lung model (75 cmH2O·s·l^-1) was relatively low, compared with established values of resistance in the intubated newborn infant with respiratory distress (120–380 cmH2O·s·l^-1) (24). Given that our in vitro studies show that P_{diff} increases with increased airway resistance, it is likely that P_{diff} may reach substantial levels at lower pressure amplitudes when an I/E of 1:2 is used in the sick intubated newborn baby. Similarly, the resistance of the ETT itself may be higher in the clinical setting, where its interior is frequently coated with secretions. The development of high-frequency ventilators with a capacity to deliver I/E ratios of 1:3 or more further increases the possibility of substantial P_{diff} occurring even at relatively low amplitude.

Importantly, the pressure difference that arises across the ETT is a rapidly achieved, steady-state phenomenon. The main clinical consequence of this phenomenon, therefore, is that whenever the mechanical characteristics of the respiratory system or ventilator settings are altered, a new lung volume will result. The magnitude of such changes in lung volume will increase as I/E ratio moves away from 1:1. Our studies show that the adoption of I/E ratios approaching 1:1 might eliminate the fluctuations in lung volume, which might otherwise result from the pressure drop across the ETT. Where I/E ratios other than 1:1 are employed, the accurate measurement of flow across the ETT would provide a means of calculating the difference in mean pressure between the airway opening and the lung.

The optimization of lung volume has been a focus of clinical HFOV strategies during the last decade. Common clinical practice involves initial setting of Pao 1–2 cmH2O higher than that employed during CMV, with increments in Pao being imposed until a substantial reduction in the inspired O2 fraction, necessary to maintain normoxia, is achieved. To date, no data are available to indicate the extent to which the Pao required in clinical practice for optimal lung recruitment may be related to the I/E ratio employed.
Although HFOV is frequently employed in the premature infant with hyaline membrane disease, which is a homogeneous lung disease, it is also used to ventilate neonates with other forms of respiratory disease. In some cases, this might be associated with a degree of ventilation inhomogeneity. Although it is likely that this scenario might create small regional differences in \( \bar{P}_A \), the pros and cons of a symmetric vs. asymmetric I/E ratio in the presence of conditions such as pulmonary interstitial emphysema remain to be tested.

In conclusion, our observations of minimal difference between \( \bar{P}_A \) and \( \bar{P}_{ao} \) at an I/E of 1:1, and the presence of a substantial difference at an I/E ratio of 1:2, call into question whether the common practice of employing an I/E ratio of 1:2 is the optimal strategy for HFOV. Whereas it may be argued that the \( \overline{P_{\text{diff}}} \) generated at an I/E ratio of 1:2 has the advantage of offsetting any tendency toward gas trapping, either due to expiratory flow limitation or reduced airway caliber in expiration, this strategy is not without potential problems. Not only does it create the potential for \( \bar{P}_A \) to be substantially different from the \( \bar{P}_{ao} \) displayed by the machine, it also creates the opportunity for changes in ventilator amplitude and frequency, or in the size of the infant’s ETT, to have quite unanticipated and undesirable effects on \( \bar{P}_A \).

**APPENDIX A**

The instantaneous pressure at the airway opening \( \bar{P}_{ao} \) is equal to the sum of the resistive and inertive pressure drops associated with the ETT (\( \bar{P}_{res} \) and \( \bar{P}_{in} \), respectively) and the alveolar pressure \( \bar{P}_A \)

\[
\bar{P}_{ao} = \bar{P}_{res} + \bar{P}_{in} + \bar{P}_A
\]  

(A1)

Integrating term by term over a full cycle and regrouping, we can write

\[
\bar{P}_A - \bar{P}_{ao} = -(\bar{P}_{res} + \bar{P}_{in})
\]  

(Note that in Eq. A2 and all that follow, the mean is taken over a complete cycle). Because \( \bar{P}_{in} = 0 \) (see APPENDIX B), and defining \( \bar{P}_A - \bar{P}_{ao} = \overline{P_{\text{diff}}} \), Eq. A2 simplifies to

\[
\overline{P_{\text{diff}}} = -\bar{P}_{res}
\]  

(A3)

When using Rohrer’s equation to represent the effects of turbulent flow in the ETT, the \( \bar{P}_{res} \) for inspiration (I) and expiration (E) is, respectively

\[
\bar{P}_{resI} = k_{1I}V_I + k_{2I}V_I^{2/3}
\]  

(A4a)

and

\[
\bar{P}_{resE} = k_{1E}V_E - k_{2E}V_E^{2/3}
\]  

(A4b)

where \( V_I \) is the flow in the ETT and \( k_{1I}, k_{2I}, k_{1E}, \) and \( k_{2E} \) are experimentally determined constants. Note that the negative sign is necessary in Eq. A4b to take account of flow reversal during expiration. Recognizing that the \( \bar{P}_{res} \) over a complete cycle is

\[
\bar{P}_{res} = \bar{P}_{resI} + \bar{P}_{resE}
\]  

(A5)

and substituting Eq. A4a and A4b into Eq. A5 gives

\[
\bar{P}_{res} = k_{1I}V_I + k_{2I}V_I^{2/3} + k_{1E}V_E - k_{2E}V_E^{2/3}
\]  

(A6)

Assuming that \( k_{1I} = k_{1E} \) and, further, that \( k_{2I} = k_{2E} = k_2 \), and recognizing that \( V_I = V_E \), Eqs. A3 and A6 yield

\[
\overline{P_{\text{diff}}} = -k_2(V_I^{2/3} - V_E^{2/3})
\]  

(A7)

Finally, rewriting Eq. A7 in terms of flow velocity \( U \) in the ETT

\[
\overline{P_{\text{diff}}} = -k_2A(U_I^{2/3} - U_E^{2/3})
\]  

(A8)

where \( A \) is the cross-sectional area of the ETT. Subject to the assumptions above, Eq. A8 indicates that the relationship between \( \overline{P_{\text{diff}}} \) and \( U_I^{2/3} - U_E^{2/3} \) is a straight line through the origin with a negative slope of \( k_2A^2 \). Calculation of \( k_2A^2 \), using averaged \( k_2 \) values derived from the inspiratory and expiratory \( k_2 \) data of Sly et al. (22) for a 10-cm-long ETT, gives \(-0.014, -0.013, \) and \(-0.011 \) for 2.5-, 3.0-, and 4.0-mm ETTs, respectively. The average calculated slope for the three ETTs is \(-0.013 \), in excellent agreement with that deduced from Fig. 4, which is \(-0.012 \).

**APPENDIX B**

The pressure drop \( P_{in} \) across the inertance (1) of the ETT is

\[
P_{in} = \int \frac{dV'}{dt}
\]  

(B1)

where \( V' \) is the instantaneous flow in the ETT.

Assuming I is invariant, the average \( P_{in} \) is, therefore

\[
P_{in} = \frac{1}{T} \int_0^T \frac{dV'}{dt} dt
\]  

(B2)

where the integration is taken over a full cycle with duration \( T \).

Evaluation of Eq. B2 gives

\[
P_{in} = \frac{1}{T} [V'(T) - V'(0)]
\]  

(B3)

If flow is periodic, so that \( V'(T) = V'(0) \), then

\[
P_{in} = 0
\]  

(B4)

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