A method for measuring and modeling the physiological traits causing obstructive sleep apnea

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A method for measuring and modeling the physiological traits causing obstructive sleep apnea. J Appl Physiol 110: 1627–1637, 2011. First published March 24, 2011; doi:10.1152/japplphysiol.00972.2010.—There is not a clinically available technique for measuring the physiological traits causing obstructive sleep apnea (OSA). Therefore, it is often difficult to determine why an individual has OSA or to what extent the various traits contribute to the development of OSA. In this study, we present a noninvasive method for measuring four important physiological traits causing OSA: 1) pharyngeal anatomy/collapsibility, 2) ventilatory control system gain (loop gain), 3) the ability of the upper airway to dilate/stiffen in response to an increase in ventilatory drive, and 4) arousal threshold. These variables are measured using a single maneuver in which continuous positive airway pressure (CPAP) is dropped from an optimum to various suboptimum pressures for 3- to 5-min intervals during sleep. Each individual’s set of traits is entered into a physiological model of OSA that graphically illustrates the relative importance of each trait in that individual. Results from 14 subjects (10 with OSA) are described. Repeatability measurements from separate nights are also presented for four subjects. The measurements and model illustrate the multifactorial nature of OSA pathogenesis and how, in some individuals, small adjustments of one or another trait (which might be achievable with non-CPAP agents) could potentially treat OSA. This technique could conceivably be used clinically to define a patient’s physiology and guide therapy based on the traits.

Theoretical Description of the Measurements and the Model

The traits are measured by placing subjects on enough CPAP during sleep to completely open the pharyngeal airway (termed the

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holding pressure) and then dropping the pressure intermittently throughout the night to subtherapeutic levels for 3- to 5-min intervals.

**Ventilatory response to disturbance measurement.** The ventilatory response-to-disturbance ratio is the loop gain of the respiratory control system. Figure 1 illustrates the concept of loop gain and how it can be measured from a CPAP drop. In this figure, a single 3-min CPAP drop is shown. During the first 30 s, CPAP is at the holding pressure and the airway is completely open. When CPAP is dropped to 5 cm H2O (in this example), ventilation decreases because the upper airway narrows. Thereafter, ventilation recovers partially due to airway stiffening and increased respiratory effort and achieves a new steady state that is below eupnea. The reduced ventilation on suboptimum CPAP [quantified as ΔVentilation (response)] leads to an accumulation of CO2 and ventilatory drive. The amount of ventilatory drive that has accumulated can be determined by returning CPAP to the holding pressure (thereby opening the airway) and measuring the ventilatory overshoot [ΔVentilation (response)]. Loop gain is the ventilatory response to disturbance ratio [Loop gain = ΔVentilation (response) / ΔVentilation (disturbance)]. Figure 1 demonstrates that if ventilation is reduced by −2.3 l/min and is allowed to reach a steady state at this level, ventilatory drive will increase by 4.2 l/min, i.e., the steady-state loop gain is −1.8. Loop gain is a negative number because the response is in the opposite direction to the disturbance.

To demonstrate how the different traits interact to produce OSA in a particular individual, they are plotted on a graph of ventilatory drive vs. ventilation. To put loop gain on this graph, the eupneic ventilation on optimum CPAP is first plotted (see the dot in Fig. 2A). Then, vectors are drawn representing the ventilatory disturbance and the ventilatory response from Fig. 1. The line connecting these vectors is the loop gain, and thus loop gain is represented as a slope on this graph. To add the other traits to the model, the x-axis and y-axis in Fig. 2A are “flipped” to produce Fig. 2B. The reason for this will become clear in the next section.

**Pharyngeal anatomy/collapsibility measurement.** The upper airway “anatomy” is quantified as the ventilation on no CPAP (atmospheric pressure) at the eupneic level of ventilatory drive. This trait is symbolized as V0 (ventilation at zero nasal pressure). V0 is determined by recording the mask pressure and ventilation at the holding pressure and at the beginning of each pressure drop and then plotting them on a graph of ventilation vs. pressure. The data are fit with a straight line, and V0 is the y-intercept (Fig. 3A). This technique is similar to the pharyngeal critical pressure measurement (29) except that ventilation, rather than inspiratory flow, is plotted on the ordinate and the x-intercept, rather than the y-intercept, is used to quantify pharyngeal collapsibility. This approach allows the anatomy parameter to be incorporated into the model using units of liters per minute. Figure 3B shows the OSA model with the loop gain and anatomy traits plotted.

**Upper airway gain measurement.** During sleep, particularly in patients with OSA, the upper airway may partially or completely obstruct, thereby reducing ventilation. As a result, PCO2 and the ventilatory drive to breathe increase. The latter will stimulate the diaphragm and upper airway muscles, and ventilation may compensate to some extent. The amount of compensation depends mostly on the ability of the upper airway to stiffen/dilate in response to the increase in drive. This ability, which we term the “upper airway gain,” is quantified from a CPAP drop as shown in Fig. 4. In this figure, the

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1 The steady-state loop gain is different from the loop gain “at the frequency associated with a phase angle of 180°,” which is what our laboratory and others have previously reported (15, 36, 41). The loop gain at the frequency associated with a 180° phase angle is a function of ventilatory control system dynamics (e.g., circulation delay, time course of the increase in CO2 after a change in ventilation). The steady-state loop gain, as the name implies, is not dependent on dynamics. Rationale for using the steady-state loop gain in the OSA model, and not the “dynamic” loop gain, is given in the online Supplement Section I.C. Note, however, that a model is presented later in the text that would allow one to calculate the loop gain at any frequency, i.e., the dynamic loop gain.
drop in CPAP from 13 to 5 cm H2O leads to an abrupt reduction in ventilation from 5.1 to 1.5 l/min. As ventilatory drive increases, ventilation also increases but generally does not achieve eupneic levels because the airway is narrowed. The increase in compensatory ventilation ($\Delta V_E$ in Fig. 4A) that occurs, divided by the increase in ventilatory drive ($\Delta$Ventilatory Drive), is the upper airway gain.2

The upper airway gain can now be added to the model. Starting at the anatomy point (square in Fig. 4B), vectors representing the $\Delta V_E$ and $\Delta$Ventilatory Drive from Fig. 4A are drawn. The dashed line connecting these vectors is the upper airway gain (see Section III.B. in the online supplement for justification for modeling the upper airway gain as a linear function of drive; Supplement Material for this article is available online at the J Appl Physiol website.). The intersection of the upper airway gain line and the 1/Loop gain line is the simultaneous solution to the equations for both lines, and it is the predicted steady-state ventilation that would occur during sleep in the absence of CPAP. Whether this level of ventilation is tolerated depends on the arousal threshold, which is described next.

**Arousal threshold measurement.** The arousal threshold is defined as the ventilatory drive that produces arousal (2, 5). With this method, ventilatory drive during the CPAP drop is calculated using a dynamic model of the ventilatory control system (this dynamic model is different from the graphical OSA model depicted in Fig. 4B). From the same tracings used to determine loop gain, one can also estimate the circulation delay and time constant of the ventilatory control system (see Fig. 5A, the details of how the delay and time constant are estimated are described below and in the online Supplement Section I.B.). Knowing the gain, delay, and time constant allows the increase in ventilatory drive at any point in the CPAP drop to be calculated. Thus, when an arousal occurs, the ventilatory drive at the time of arousal can be determined (Fig. 5B).

The arousal threshold is added to the OSA model by placing a vertical line at the ventilatory drive that produces arousals (Fig. 6). The model is now complete and indicates that the subject will probably have OSA for the following reason: during sleep in the absence of CPAP.

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2 Ventilation during a CPAP drop (divided by the increase in ventilatory drive) could increase for reasons other than pharyngeal stiffening/dilation, namely from changes in breath timing or the inspiratory flow shape (39). However, it is referred to as the upper airway gain for simplicity.

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**Fig. 3.** A: determination of $V_0$. Ventilation at several levels of mask pressure is plotted (□) and fit with a straight line. The anatomy trait is the ventilation at zero mask pressure (●), which is 0.7 l/min in this example. B: model with the upper airway anatomy and loop gain plotted. To plot $V_0$ in the model, the eupneic level of ventilatory drive is found on the x-axis (5.1 l/min) and a closed square is placed at a ventilation of 0.7 l/min.

**Fig. 4.** A: measurement of the upper airway gain from a CPAP drop. As in Fig. 1, a single 3-min drop is shown. The increase in ventilation across the drop ($\Delta V_E$) is divided by the increase in ventilatory drive ($\Delta$Ventilatory Drive) to get the upper airway gain. In this example, the upper airway gain is 1.3 l/min $\div$ 4.2 l/min, which equals 0.31. The OSA model, with the addition of the upper airway gain, is shown in B. Starting at the anatomy point (●), the upper airway gain (dashed line) is plotted by drawing vectors for the increase in ventilatory drive and the resulting increase in ventilation (justification for plotting the upper airway gain starting at the anatomy point, $V_0$ is given in the online Supplement Section III.A.). The intersection of the solid (1/Loop gain) and dashed (upper airway gain) lines is the predicted steady-state ventilation off CPAP (this intersection is termed the “steady-state point”). The model indicates that, in the absence of CPAP, ventilation will increase as a function of increasing ventilatory drive until it reaches a steady-state level at 2.2 l/min.
absence of CPAP, ventilation is initially 0.7 l/min. As ventilatory drive increases, ventilation increases (approximately) along the upper airway gain line. However, before it intersects the loop gain line, an arousal occurs. Therefore, according to the model, if the steady-state point (intersection of the dashed line and the solid line) is to the right of the arousal threshold line, then OSA will occur. If the steady-state point is to the left of the arousal threshold line, then OSA will not occur. Figure 6B shows how small manipulations in the traits might bring the steady-state point into the stable region (to the left of the arousal threshold line).

Of note, the OSA model in Fig. 6 is a steady-state model. There is no time axis, and hence the dynamics of the ventilatory control system.

Fig. 5. Determination of the arousal threshold from a CPAP drop. A: same CPAP drop as that shown in Figs. 1 and 4A. As described in Fig. 1, the steady-state loop gain is calculated by dividing the response by the disturbance. The dynamics of the ventilatory control system (Delay and time constant) are estimated from the time course of the decline in ventilation after the overshoot. The dotted line is the calculated increase in ventilatory drive determined from a dynamic model of the ventilatory control system (described later in the text and in detail in the online Supplement Section I.B.). B: CPAP drop that produces an arousal. The solid line is the ventilation, and the dotted line is the calculated ventilatory drive. At 70 s, an arousal occurs. Ventilatory drive at arousal, which defines the arousal threshold, is 9 l/min.

Fig. 6. A: OSA model with all 4 traits plotted. Arousal threshold (dashed line) is added by moving along the x-axis and placing a vertical line at 9 l/min. The model indicates that, off CPAP, an arousal will occur before stable breathing can be achieved, i.e., the subject will have OSA. Diagram B illustrates the potential clinical usefulness of the model and suggests that slight adjustments in the anatomy point (moving the square vertically upwards from 0.7 to 1.7 l/min, as might occur with weight loss or pharyngeal surgery) and the arousal threshold (shifting the dotted line to the right by 1 l/min, as might be achievable with a sedative) may move the intersection of the solid and dashed lines from the right (unstable region) to the left (stable region) of the arousal threshold line and eliminate or substantially reduce apnea.
(delay and time constant) cannot be easily depicted. Consequently, the frequency of cycling and other dynamic features cannot be constrained. There are strengths and weaknesses to this approach. The primary strengths are: 1) the steady-state loop gain is important for determining whether stable (steady state) ventilation can occur during sleep without arousals, and 2) the traits can be plotted on a graph that allows their interrelationships to be appreciated. The major weakness is that, under certain conditions, the dynamics can affect the interpretation of the steady-state model. These conditions are described in the online Supplement Section I.C.

Subjects

The normal controls were recruited from the community and had an apnea-hypopnea index (AHI) <10/h during supine non-rapid eye movement (NREM) sleep. CPAP-adherent OSA patients with an AHI >10/h during supine NREM sleep were recruited from our clinical sleep center. Adherence was defined as a compliance factor 

Subjects slept in the supine position and breathed through the nasal mask connected via a breathing circuit to a positive/negative pressure source (modified CPAP machine; Philips Respironics). The mouth was taped shut to reduce leaks. Once aslee, CPAP was set to the holding pressure, defined as the mask pressure required to eliminate hypopneas, snoring, and flow limitation (flattened inspiratory flow). After several minutes of stable breathing at the holding pressure, CPAP was abruptly decreased for 3–5 min and then returned to the holding pressure for another 3–5 min. These maneuvers were repeated multiple times throughout the night to varying levels of CPAP or continuous negative airway pressure in random order. If awakening occurred during a drop, the pressure was returned to the holding pressure until sleep resumed and subsequent drops could be performed. The physiological traits were estimated from data obtained during supine NREM sleep.

Data analysis

Loop gain. The raw flow signals were integrated to get volume. Unintentional (e.g., mask) leaks were removed by fitting a regression line to the volume signal. The slope of this line is the leak, which was subtracted from the flow signal before reinserting it to get the corrected tidal volume. This was done for each level of mask pressure.

The loop gain, time constant, and delay (as labeled in Fig. 5A) were estimated from the last 60 s of a drop (in which CPAP was at a subtherapeutic level) plus the subsequent 3 min immediately succeeding the drop (in which CPAP was at the holding pressure). In order for a drop to be considered for loop gain measurement, ventilation during the last 60 s of the drop had to be significantly less (P < 0.1) than eupneic ventilation on optimum CPAP. Also, no arousals could occur during this interval. Each signal meeting these criteria was scaled so that the disturbance magnitude (ΔVentilation (disturbance)) in Fig. 1] equaled 1 l/min. This scaling was done so that the different drops (which had different disturbance amplitudes) could be ensemble averaged to reduce noise (see the online Supplement Section I.A. for more details). The ensemble averaged signal was fit to the model equation below, which is a transfer function model written as a function of complex frequency (the model is described in detail in the online Supplement Section I.B.).

\[ G_l(s) = \frac{\Delta V_{drive}(s)}{\Delta V_{E(s)}} = \frac{G_l}{\tau_s + 1} e^{-sD} \]

\[ G_l(s) \] is the loop gain as a function of complex frequency. The \( s \) is the symbol used to denote complex frequency. \( \Delta V_{drive}(s) \) is the change in ventilatory drive, or the response, as a function of complex frequency. \( \Delta V_{E(s)} \) is the change in ventilation, or the disturbance, as a function of complex frequency. \( G_l \) is the steady-state loop gain, which is the ventilatory response to a steady-state disturbance. This is the ratio defined in Fig. 1. \( D \) is the circulation delay between the pulmonary capillaries and the peripheral chemoreceptors. In the complex frequency domain, time delays are modeled as exponential functions, hence the term \( e^{-sD} \). \( \tau \) is the time constant for the ventilatory control system. To estimate the steady-state loop gain (\( G_l \)) and dynamics (\( D \) and \( \tau \)), we need to know the input, \( \Delta V_{E(s)} \), and the output, \( \Delta V_{drive}(s) \), to the equation. \( \Delta V_{E(s)} \) is obtained from the measured flow signal. \( \Delta V_{drive}(s) \) is determined by extrapolating the ventilatory overshoot backwards, as depicted in Fig. 7 [more detail about how \( \Delta V_{E(s)} \) and \( \Delta V_{drive}(s) \) were obtained is given in the online Supplement Section I.A.]. The parameters (\( G_l \), \( D \), and \( \tau \)) were determined by inputting \( \Delta V_{E(s)} \) into the equation and then “tuning” \( G_l \), \( D \), and \( \tau \) using least squares regression to make the model output fit the measured signal.
pressure (obtained from each 1-min segment of data before each CPAP drop); and 2) the mask pressure and ventilation of the second and third breath of each pressure drop. The first breath was not used as it often is not reduced as much as the second and third breath of each pressure drop. The first breath was not used because the ventilatory drive would likely have increased by this time, and we wanted V_o to reflect the ventilation at eupneic ventilatory drive. The data were then fit with a straight line, and the y-intercept was taken as V_o.

Upper airway gain. The upper airway gain was calculated from runs that did not end in arousal. The upper airway gain is a ratio (ΔVentilation/ΔVentilatory Drive), as shown in Fig. 4A. The numerator (ΔVentilation) is the increase in ventilation across the drop, and it was calculated by subtracting the mean ventilation on the last three breaths of the drop by the mean ventilation of breaths 2 and 3 of the drop. The denominator (ΔVentilatory Drive) is the increase in ventilatory drive across the CPAP drop, and it was calculated by subtracting the mean ventilation of the first two breaths of the ventilatory overshoot (after CPAP was returned to the holding pressure) by the eupneic ventilation on optimum CPAP (see the online Supplement Section III for a detailed illustration of this calculation). The different responses were averaged to determine the mean upper airway gain in an individual.

Arousal threshold. Arousals, defined as a high frequency shift in EEG for >3 s, were scored by an experienced technologist, with particular attention paid to the start and end of each arousal. To estimate the arousal threshold, the increase in ventilatory drive was calculated using the G_t, D, and τ. Because many drops do not end in an arousal, and because the ventilatory drive achieved on these drops is sometimes higher than those that do end in arousal (arousal threshold is variable), the arousal threshold was estimated using survival analysis (40) (see the online Supplement Section II). From a survival analysis plot like the one shown in Fig. 8A, the arousal threshold was taken as the ventilatory drive at which there is a 50% probability of arousal.

RESULTS

The subjects’ characteristics are shown in Table 1. Four individuals (subjects 1–4) did not have significant OSA in NREM sleep. Subject 3 used CPAP at home for REM-related OSA. The average CPAP used at home was 9 ± 3 cm H2O. Most subjects were middle aged (47 ± 12 yr old) and obese (body mass index = 34 ± 7 kg/m2). There was a large range of AHIs from 0 to 115 episodes/h.

Figure 7. Back extrapolation from the peak of the overshoot is used to construct the ventilatory drive signal (dotted line) during the last 60 s of the CPAP drop (from 150 to 210 s). After the CPAP drop, from 210 s onwards, the ventilation matches the ventilatory drive (because the airway is open and there is no longer any impediment to ventilation) and the dotted and solid lines equal one another. There are now two signals: the solid line, which is the pneumotach-measured ventilation signal that is the input to the transfer function model, ΔVE(s); and the dotted line, which is the derived ventilatory drive signal that is the output of the model, ΔV_drive(s). Online Supplement Section I.A. describes in detail the justification for this “back extrapolation” procedure.

Figure 8 shows representative examples of raw data used to determine the physiological traits in several subjects. Figure 8B displays the changes in ventilation when CPAP was returned to the holding pressure in one subject. These data were used for calculating loop gain. Multiple drops to different levels of nasal pressure were performed in this individual, but the signals have been scaled (such that the difference between eupneic ventilation and the reduced ventilation during the drop is 1 l/min) and shifted (so that the baseline is 0 l/min). The signals from each run overlay one another, indicating that loop gain is linear in the ranges tested. To reduce the noise before estimating the loop gain, delay, and time constant, these signals were ensemble averaged.

Figure 8C is the ventilation at each level of nasal pressure (including the holding pressure) for a single subject. These data were used for calculating V_o. In this individual, 21 CPAP drops were performed. The holding pressure was 6 cm H2O, which produced 21 data points at this pressure level (this is the eupneic ventilation). The open squares at each pressure level are the average of the second and third breaths of each CPAP drop. The V_o in this patient is 2.8 l/min.

Figure 8D displays the changes in ventilation as a function of increasing ventilatory drive in one subject. These data were used for calculating the upper airway gain. The dots on the left correspond to the ventilation on breaths 2 and 3 of each drop, and the dots on the right correspond to the ventilation for the last three breaths of the drop. Thus there are two dots connected by a line for each drop. The average upper airway gain in this patient is 0.64.

Model Results for Each Subject

The model diagrams in Fig. 9 suggest that OSA can occur, or not occur, for different reasons in different individuals [subjects 1–10 are shown in Fig. 9 and subjects 11–14 (repeatability data) are shown in Fig. 10]. Subject 1 has a low/normal loop gain, a V_o that is only slightly below eupneic ventilation, and a positively sloped upper airway gain, all of which protect against OSA. Thus, while the arousal threshold is the lowest of the 10 individuals shown here (which would increase the probability of having respiratory effort-related arousals), sub-
Subject 1 does not have OSA. In subject 2, the combination of a low loop gain and positive upper airway gain is probably the most important trait preventing OSA. Subject 3 has a very high loop gain, a low $V_0$, and a low arousal threshold. If only these three traits were measured, one might predict that this patient has OSA. However, the upper airway gain is very positive and clearly protective in this individual. Subject 4 also has a very positive upper airway gain, which in combination with a low loop gain, is enough to overcome the poor anatomy and low arousal threshold.

Subjects 5 and 6 have mild OSA. The possible cause of OSA in subject 5 is interesting. Note that the anatomy point ($V_0$) in this subject is greater than in the preceding three individuals. Also, the loop gain is low, the arousal threshold is high, and the upper airway gain is positively sloped. It would be expected, therefore, that this patient would not have OSA. However, the eupneic ventilation is substantially elevated, thereby making it harder for the loop gain line to intersect the upper airway gain line in the stable region (to the left of the arousal threshold line). In this regard, the eupneic ventilation plays a similar role to the $V_0$. In subject 6, the relatively high loop gain and low $V_0$ are probably the important traits that contribute to mild OSA in this patient.

Subjects 7–10 have severe OSA. In subject 7, the loop gain and upper airway gain are variable and not well characterized by a mean slope. Nevertheless, it seems that the mostly negative upper airway gain and low arousal threshold are contributing to OSA in this individual. Note that the anatomy points are similar in subjects 7 and 1, yet the AHI are substantially different. Subject 8 has a normal loop gain, a slightly positive upper airway gain, and a normal arousal threshold. However, the $V_0$ is markedly reduced and has a negative value. While it is impossible to have negative ventilation, a negative $V_0$ means that the airway will be closed off of CPAP and will remain closed until the ventilatory drive increases enough to reopen it (which is $\sim 20$ l/min in this individual). In subjects 9 and 10, the major mechanism causing

Table 1. Subject characteristics

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Values are means ± SD. BMI, body mass index; CPAP, continuous positive airway pressure; AHI, apnea-hypopnea index; NA, not applicable. *Home use. †Supine, non-rapid eye movement sleep.
OSA is the negative upper airway gain. Such a response makes the possibility of achieving stable breathing during sleep virtually impossible, regardless of the other traits. Note that subject 9 has a normal $V_0$ and a high arousal threshold, and subject 10 has a low loop gain and a high arousal threshold. Nevertheless, both clearly have OSA. These diagrams illustrate the importance of interpreting the physiological traits in relationship to one another.

Fig. 9. Model results and AHI for subjects 1–10 (subjects 11–14 are shown in Fig. 10). As in the previous diagrams, eupneic ventilation is marked by the dot, $V_0$ by the square, the reciprocal of loop gain by the solid line, the upper airway gain by the dashed line, and the arousal threshold by the vertical dotted line. Values for each trait are listed in the top left of each graph. $V_E$, ventilation on optimum CPAP; $G_L$, loop gain; $V_0$, ventilation at zero nasal pressure and eupneic ventilatory drive; $T_A$, arousal threshold in l/min; $G_{UA}$, upper airway gain. The 90% confidence intervals are marked by shading.
Repeatability of the measurements. Figure 10 shows night-to-night repeatability data in four subjects. In subject A, the traits are similar on both nights except for the arousal threshold, which is 3.2 l/min higher on night 2. In subject B, the parameters are virtually the same on both nights. Subject C has an ~1 l/min higher ventilation on night 2, and all of the other traits are slightly higher as well, but not by much, and the physiology is generally the same: there is a negative upper
airway gain without bad anatomy (V0 is 1.5–2 l/min less than euepine ventilation), a moderately high loop gain, and a medium arousal threshold. In subject D, the traits mostly agree except for V0, but again the major physiology (mild anatomical abnormality with significantly negative upper airway gain) is captured. These data suggest that the measurements of the traits are generally repeatable from night to night.

**DISCUSSION**

In this study, a noninvasive technique for measuring several physiological traits that contribute to the pathogenesis of OSA is presented. The technique involves raising and lowering CPAP and measuring the resultant changes in ventilation. This is a relatively simple methodology that could be used in a clinical laboratory. A model of OSA pathogenesis that incorporates the measured traits is also presented. The model illustrates in a concise diagram how the traits interact to produce or prevent OSA.

The purpose for developing this technique is to provide clinicians and patients with additional potential treatment options. Currently, most OSA patients are prescribed CPAP, which is effective but has an acceptance rate of only ~50% (4, 16). If, however, the contribution of each trait could be determined in a particular patient, then it might be possible to target the abnormal traits and treat OSA without CPAP in some individuals. For example, upper airway surgery and a sedative might be effective in a patient with a small/narrow upper airway and a low arousal threshold. If the ventilatory control system is also unstable, then adding oxygen or acetazolamide (which stabilize the ventilatory control system; Refs. 17, 22, 26, 32, 35) might be useful as well. Also, if drugs that stimulate the upper airway muscles are developed, they will likely need to be combined with other therapies to fully treat the OSA.

A number of investigators have already studied the effects of non-CPAP therapies [e.g., uvulopalatopharyngoplasty (30), oral appliances (10, 23), oxygen (6, 7, 18, 33), acetazolamide (11, 28, 31, 34, 37), and sedatives (3, 9, 27)] on apnea severity and, in a limited fashion, the physiological traits themselves. These studies were performed in largely unselected populations. In most cases, the agents, when tested, altered/improved the trait; however, the effect on AHI was generally modest, although some patients exhibited more complete responses. We believe that better matching of the agent (or combinations of agents) with the mechanisms causing OSA will lead to better results.

As an example of how the model might help in this process, consider the model diagrams in Fig. 9 again. In subject 5, the only abnormal trait is the high ventilatory demand. Thus it might be possible for this patient to achieve stable breathing during sleep by lowering the metabolic rate. In subject 6, lowering the loop gain and raising V0 using some of the interventions described above might eliminate OSA. Subject 7 has a low arousal threshold. This would seem a reasonable therapeutic target. However, unless the negative upper airway gain is also addressed (if future drugs make this possible), raising the arousal threshold is unlikely to be effective. Similarly, lowering the relatively high loop gain in subject 9 would probably also need to be combined with an improvement in the upper airway gain (the upper airway gain is undoubtedly an important trait that needs to be more completely understood).

Lastly, subjects 8 and 10 probably require CPAP, as it is unlikely that small adjustments in the traits could allow the patients to achieve stable breathing. Clearly, knowledge regarding how much a particular trait could be adjusted would be helpful in making this decision.

**Limitations**

There are a number of limitations that must be kept in mind when considering this study. 1) In this study, the “validation” of the overall approach is whether or not the complete set of measured traits predicts OSA (or no OSA) when incorporated into the model. This was accomplished, as we correctly predicted the presence or absence of OSA in all 14 subjects. However, we recognize that each measurement should be validated independently, and this is planned in future experiments. 2) All of the determinations in this study were obtained from supine, NREM sleep, and thus they cannot be extrapolated to REM sleep. Measurement of traits during REM sleep is challenging due to REM-related breathing variability and insufficient time in REM sleep. However, such testing may be needed. 3) The measurements are noisy, which is likely due to intrinsic variability in the physiology as well as measurement noise. In most cases, multiple measurements were made to “average out” the noise. However, the requirement that ventilation reach a steady state during the CPAP drop (to measure loop gain, see Fig. 1) limited the number of measurements that could be made in a single night. The model would be improved if the traits could be estimated from shorter drops, which would allow for more measurements and greater confidence in the estimates. 4) The frequency of events as a measure of OSA severity might not be predicted well by a steady-state model such as the one described in this study. Thus, while it can be used to predict if someone will have OSA, it might not correlate well with the AHI in all individuals. Despite these limitations, this approach may have both diagnostic and potentially therapeutic value. Future studies of the effect of non-CPAP agents on the traits are needed, as is testing of combination therapy in which agents are matched with the abnormal traits.

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**REFERENCES**
